FLUID MECHANICS D203 SAE SOLUTIONS TUTORIAL 3 – BOUNDARY LAYERS

SELF ASSESSMENT EXERCISE 1

1. A smooth thin plate 5 m long and 1 m wide is placed in an air stream moving at 3 m/s with its length parallel with the flow. Calculate the drag force on each side of the plate. The density of the air is 1.2 kg/m^3 and the kinematic viscosity is $1.6 \times 10^{-5} \text{ m}^2/\text{s}$.

$$\begin{split} R_{ex} &= u \; L/v = 3 \; x \; 5/1.6 \; x \; 10^{-5} = 937.5 \; x \; 10^3 \\ C_{DF} &= 0.074 \; R_{ex}^{-1/5} = 4.729 \; x \; 10^{-3} \\ Dynamic \; Pressure &= \rho u_o^{-2}/2 = 1.2 \; x \; 3^2/2 = 5.4 \; Pa \\ \tau_w &= C_{DF} \; x \; dyn \; press = 0.0255 \; Pa \\ R &= \tau_w \; x \; A = 0.0255 \; x \; 5 = 0.128 \; N \end{split}$$

2. A pipe bore diameter D and length L has fully developed laminar flow throughout the entire length with a centre line velocity u_o . Given that the drag coefficient is given as $C_{Df} = 16/\text{Re}$ where $\text{Re} = \frac{\rho u_o D}{\mu}$, show that the drag force on the inside of the pipe is given as $\text{R}=8\pi\mu u_o\text{L}$ and hence the pressure loss in the pipe due to skin friction is $p_L = 32\mu u_o\text{L}/D^2$

$$\begin{split} &C_{DF} = 16/R_e \\ &R = \tau_w \; x \; \rho u_o{}^2/2 = C_{DF} \; x \; (\rho u_o{}^2/2) \; x \; A \\ &R = (16/R_e)(\rho u_o{}^2/2) \; A \\ &R = (16\mu/\rho u_o D)(\rho u_o{}^2/2) \; \pi DL \\ &R = (16 \; \mu \; u_o \; \pi \; L/2) = 8 \; \pi \; \mu \; u_o \; L \\ &p_L = R/A = 8 \; \pi \; \mu \; u_o \; L \; / (\pi D^2/4) = 32 \; \mu \; u_o \; L/D^2 \end{split}$$

SELF ASSESSMENT EXERCISE No. 2

 Calculate the drag force for a cylindrical chimney 0.9 m diameter and 50 m tall in a wind blowing at 30 m/s given that the drag coefficient is 0.8. The density of the air is 1.2 kg/m³.

 $C_D = 0.8 = 2R/(\rho u^2 A)$ $R = 0.8 (\rho u^2/2)A = 0.8 (1.2 \text{ x } 30^2/2)(50 \text{ x } 0.9) = 19440 \text{ N}$

2 Using the graph (fig.1.12) to find the drag coefficient, determine the drag force per metre length acting on an overhead power line 30 mm diameter when the wind blows at 8 m/s. The density of air may be taken as 1.25 kg/m^3 and the kinematic viscosity as $1.5 \times 10^{-5} \text{ m}^2/\text{s}$. (1.8 N).

$$\label{eq:Re} \begin{split} R_e &= u \; d/\nu = 8 \; x \; 0.03/1.5 \; x \; 10^{-5} = 16 \; x \; 10^3 \\ \text{From the graph} \\ C_D &= 1.5 \end{split}$$

 $R = C_D (\rho u_o^2/2) A = 1.5 (1.25 \text{ x } 8^2/2)(0.03 \text{ x } 1) = 1.8 \text{ N}$

SELF ASSESSMENT EXERCISE No. 3

1. a. Explain the term Stokes flow and terminal velocity. b. Show that the terminal velocity of a spherical particle with Stokes flow is given by the formulae = $d^2g(\rho_s - \rho_f)/18\mu$. Go on to show that $C_D=24/R_e$

 $\begin{array}{l} \mbox{Stokes flow -for ideal fluid - no separation - Re <0.2} \\ R = Buoyant weight = (\pi d^3/6)g \ (\rho_s - \rho_f) = 3 \ \pi \ d \ \mu \ u_t \\ u_t = d^2 \ g \ (\rho_s - \rho_f)/18 \ \mu \qquad \qquad R = C_D(\rho \ u_t^2/2)(\pi \ d^2/4) \\ \end{array} \right. \qquad \qquad C_D = 26 \mu/(\rho \ u_t \ d) = 24/R_e$

2. Calculate the largest diameter sphere that can be lifted upwards by a vertical flow of water moving at 1 m/s. The sphere is made of glass with a density of 2630 kg/m³. The water has a density of 998 kg/m³ and a dynamic viscosity of 1 cP.

$$\begin{split} C_D = & (2/\rho \ u^2 A) R = \{(2 \ x \ 4)/ \ (\rho \ u^2 \ \pi d^2)\} \ (\pi d^3/6) g \ (\rho_s - \rho_f) = 21.38 \ d \\ \text{Try Newton Flow first} \\ D = & 0.44/21.38 = 0.206 \ m \\ R_e = & (998 \ x \ 1 \ x \ 0.0206)/0.001 = 20530 \ \text{therefore this is valid.} \end{split}$$

3. Using the same data for the sphere and water as in Q2, calculate the diameter of the largest sphere that can be lifted upwards by a vertical flow of water moving at 0.5 m/s. (5.95 mm).

 $C_D = 85.52 \text{ d} \\ D = 0.44/85.52 = 0.0051 \text{ R}_e = (998 \text{ x } 0.5 \text{ x } 0.0051)/0.001 = 2567 \text{ therefore this is valid.}$

4. Using the graph (fig. 1.12) to obtain the drag coefficient of a sphere, determine the drag on a totally immersed sphere 0.2 m diameter moving at 0.3 m/s in sea water. The density of the water is 1025 kg/m³ and the dynamic viscosity is 1.05 x 10⁻³ Ns/m².

 R_e = (pud/µ) =(1025 x 0.3 x 0.2/1.05 x 10⁻³) = 58.57 x 10³ From the graph C_D = 0.45 R = C_D (pu²/2)A = 0.45(1025 x 0.3²/2)(π x 0.2²/4) = 0.65 N

5. A glass sphere of diameter 1.5 mm and density 2 500 kg/m³ is allowed to fall through water under the action of gravity. The density of the water is 1000 kg/m³ and the dynamic viscosity is 1 cP.

Calculate the terminal velocity assuming the drag coefficient is $C_D = 24 R_e^{-1} (1 + 0.15 R_e^{-0.687})$

 $C_D = F/(Area \times Dynamic Pressure)$

$$R = \frac{\pi d^3 g(\rho_s - \rho_f)}{6} \qquad C_D = \frac{\pi d^3 g(\rho_s - \rho_f)}{(\pi d^2/4)(\rho u^2/2)} \qquad C_D = \frac{4d^3 g(\rho_s - \rho_f)}{3\rho_f u^2 d^2}$$

Arrange the formula into the form $C_D R_e^2$ as follows.

$$C_{D} = \frac{4d^{3}g(\rho_{s} - \rho_{f})}{3\rho_{f} u^{2}d^{2}} x \frac{\rho_{f}\mu^{2}}{\rho_{f}\mu^{2}} = \frac{4d^{3}g(\rho_{s} - \rho_{f})\rho_{f}}{3\mu^{2}} x \frac{\mu^{2}}{\rho_{f}^{2}u^{2}d^{2}} = \frac{4d^{3}g(\rho_{s} - \rho_{f})\rho_{f}}{3\mu^{2}} x \frac{1}{R_{e}^{2}}$$

 $C_{D}R_{e}^{2} = \frac{4d^{3}g(\rho_{s} - \rho_{f})\rho_{f}}{3\mu^{2}} \text{ and evaluating this we}$ get 66217 From $C_{D} = \frac{24}{R_{e}} \left[1 + 0.15R_{e}^{0.687} \right]$ we may solve by plotting $C_{D}R_{e}^{2}$ against Re From the graph $R_{e} = 320$ hence $u = R_{e} \mu/\rho d = 0.215 \text{ m/s}$



6. A glass sphere of density 2 690 kg/m³ falls freely through water. Find the terminal velocity for a 4 mm diameter sphere and a 0.4 mm diameter sphere. The drag coefficient is

 $C_{D} = 8F/\{\pi d^{2}\rho u^{2}\}$ This coefficient is related to the Reynolds number as shown for low values of Re. 30 Re 15 20 25 35 C_{D} 3.14 2.61 2.33 2.041.87 The density and viscosity of the water is 997 kg/m³ and 0.89 x 10^{-3} N s/m². For Re $>1000 C_D = 0.44$

For a 4 mm sphere we might guess from the question that $\,R_e$ is greater than 1000 and hence $C_D = 0.44$

$$R = \frac{\pi d^{3}g(\rho_{s} - \rho_{f})}{6} \quad C_{D} = \frac{\pi d^{3}g(\rho_{s} - \rho_{f})}{(\pi d^{2}/4)(\rho u^{2}/2)} \quad C_{D} = \frac{4d^{3}g(\rho_{s} - \rho_{f})}{3\rho_{f} u^{2}d^{2}}$$
$$u = \sqrt{\frac{4d^{3}g(\rho_{s} - \rho_{f})}{3\rho_{f} C_{D}d^{2}}} \text{Putting in values } \rho = 997 \quad \mu = 0.0089 \quad d = 0.004 \quad C_{D} = 0.44$$
$$u = 0.45 \text{ m/s} \quad \text{Check } R_{e} = \rho ud/\mu = 2013 \text{ so this is valid}$$

For the 0.4 mm sphere we might guess from the question that $C_D = \frac{8F}{\pi d^2 \rho u^2}$

$$C_{\rm D} = \frac{8F}{\pi d^2 \rho u^2} x \frac{\rho \mu^2}{\rho \mu^2} = \frac{8F\rho}{\pi \mu^2} x \frac{\mu^2}{\rho^2 u^2 d^2} = \frac{8F\rho}{\pi \mu^2} x \frac{1}{R_e^2}$$





7. A glass sphere of diameter 1.5 mm and density 2 500 kg/m³ is allowed to fall through water under the action of gravity. Find the terminal velocity assuming the drag coefficient is $C_{\rm p} = 24 \text{ Re}^{-1}(1+0.15 \text{ Re}^{0.687})$

$$R = \frac{\pi d^{3}g(\rho_{s} - \rho_{f})}{6} \text{ (The buoyant weight)}$$

$$R = \frac{\pi x \ 0.0015^{3} \ x \ 9.81(2500 - 997)}{6} = 26.056 \ x \ 10^{-6} \ N$$

$$C_{D} = \frac{8F}{\pi d^{2}\rho u^{2}} = \frac{8 \ x \ 26 \ x \ 10^{-6}}{\pi (0.0015)^{2} \ x \ 997 \ x \ u^{2}} = \frac{29.578 \ x \ 10^{3}}{u^{2}}$$

$$C_{D} = \frac{29.578 \ x \ 10^{3}}{u^{2}} = \frac{24}{R_{e}} \left[1 + 0.15 R_{e}^{0.687}\right]$$

$$\frac{29.578 \ x \ 10^{3}}{u^{2}} = \frac{24 \ x \ 0.00089}{997 \ u \ (0.0015)} \left[1 + 0.15 \left(\frac{997 \ u \ (0.0015)}{0.00089}\right)^{0.687}\right]$$

$$2.0709 = u \left[1 + 24.657 u^{0.687}\right] = u + 24.657 u^{1.687}$$

Solve for u and u = 0.215 m/s (plotting might be the best way)