TUTORIAL 7 – STABILITY ANALYSIS

This tutorial is specifically written for students studying the EC module D227 – Control System Engineering but is also useful for any student studying control.

On completion of this tutorial, you should be able to do the following.

- Explain the basic definition of system instability.
- Explain and plot Nyquist diagrams.
- Explain and calculate gain and phase margins.
- Explain and produce Bode plots.

The next tutorial continues the study of stability.

If you are not familiar with instrumentation used in control engineering, you should complete the tutorials on Instrumentation Systems.

In order to complete the theoretical part of this tutorial, you must be familiar with basic mechanical and electrical science.

You must also be familiar with the use of transfer functions and the Laplace Transform (see maths tutorials).
1. **INSTABILITY**

Consider a system in which the signals are added instead of subtracted by the summer. This is positive feedback. The electronic amplifier shown is an example of this.

![Diagram of an electronic amplifier with positive feedback](image)

We may derive the closed loop transfer function as follows.

\[
G_1 = \frac{\theta_c}{\theta_e} = \theta_i + G_2\theta_o \\
G_1(\theta_i + G_2\theta_o) = \theta_o \\
G_1\theta_i + G_1G_2\theta_o = \theta_o \\
G_1\theta_i = \theta_o G_1 + G_2\theta_o \\
G_1\theta_i = \theta_o (1 - G_1G_2) \\
G_{cl} = \frac{\theta_o}{\theta_i} = \frac{G_1}{1 - G_1G_2}
\]

If \(G_1 G_2 = 1\) then \(G_{cl} = \infty\) and the system is unstable. If \(G_1 G_2 < 1\) then \(G_{cl}\) has a finite value which is small or large depending on the values. In the electronic amplifier, the gain can be controlled by adjusting the feedback resistor (attenuator).

Suppose \(G_1 = 1\) and \(G_2 = 0.8\)  \(G_{cl} = 1/(1-0.8) = 5\)

Suppose \(G_1 = 1\) and \(G_2 = 0.99\)  \(G_{cl} = 1/(1-0.99) = 100\)

The closer the value of \(G_2\) is to 1 the higher the overall gain. It is essential that \(G_2\) is an attenuator if the system is not to be unstable.

A system designed for negative feedback with a summer that subtracts should be stable but when the signals vary, such as with a sinusoidal signal, it is possible for them to become unstable.

Consider an automatic control system such as the stabilisers on a ship. When the ship rolls, the stabilisers change angle to bring it back before the roll becomes uncomfortably large. If the stabilisers moved the wrong way, the ship would roll further. This should not happen with a well designed system but there are reasons and causes that can make such a thing happen. Suppose the ship was rolling back and forth at its natural frequency. All ships should have a righting force when they roll because of the buoyancy and will roll at a natural frequency defined by the weight, size and distribution of mass and so on. The sensor detects the roll and the hydraulic system is activated to move the stabiliser fins. Suppose that the hydraulics move too slow (perhaps a leak in the line) and by the time the stabilisers have responded, the ship has already righted itself and started to roll the other way. The stabilisers will now be in the wrong position and will make the ship roll even further. The time delay has made matters worse instead of better and this is basically what instability is about.

Another example of positive feedback is when you place a microphone in front of a loud speaker and get a loud oscillation. Another example is when you push a child on swing. If you give a small push at the start of each swing, the swing will move higher and higher. You are adding energy to the system, the opposite affect of damping. If you stop pushing, friction will slowly bring it back to rest.

With positive feedback, energy is added to the system making the output grow out of control. A system would not be designed with positive feedback but when a sinusoidal signal is applied, it is possible for the negative feedback to be converted into positive feedback. This occurs when the phase shift of the feedback is 180° to the input and the gain of the system is one or more. When this happens, the feedback reinforces the error instead of reducing it.
2. **NYQUIST DIAGRAMS**

A system with negative feedback becomes unstable if the signal arriving back at the summer is larger than the input signal and has shifted 180° relative to it. Consider the block diagram of the closed loop system. A sinusoidal signal is put in and the feedback is subtracted with the summer to produce the error. Due to time delay the feedback is 180° out of phase with the input. When they are summed the result is an error signal larger than the input signal. This will produce instability and the output will grow and grow.

![Diagram of closed loop system with feedback](image)

**Figure 2**

A method of checking if this is going to happen is to disconnect the feedback at the summer and measure the feedback over a wide range of frequencies.

![Diagram of open loop system](image)

**Figure 3**

If it is found that there is a frequency that produces a phase shift of 180° and there is a gain in the signal, then instability will result. The Nyquist diagram is the locus of the open loop transfer function plotted on the complex plane. If a system is inherently unstable, the Nyquist diagram will enclose the point -1 (the point where the phase angle is 180° and unity gain).

Consider the following system.

![Diagram of system with open loop transfer functions](image)

**Figure 4**
The transfer function relating \( \theta_i \) and \( \theta \) is 
\[
G(s) G_1 x G_2 x G_3 = \frac{K}{s(1+s)(1+2s)}.
\]
Converting this into a complex number \((s = j\omega)\) we find
\[
G(j\omega) = \frac{K\{-3\omega^2\}}{9\omega^4 + (\omega - 2\omega^3)} - j\frac{K(\omega - 2\omega^3)}{9\omega^4 + (\omega - 2\omega^3)}
\]

The polar plot below (Nyquist Diagram) is shown for \( K = 1 \) and \( K = 0.4 \). We can see that at the 180° position the radius is less than 1 when \( K = 1 \) so the system will be stable. When \( K = 2 \) the radius is greater than 1 so the system is unstable. We conclude that turning up the gain makes the system become unstable.

The plot will cross the real axis when \( \omega = 2\omega^3 \) or \( \omega = 0.707 \) and this is true for all frequencies. The plot will enclose the -1 point if
\[
\frac{K\{-3\omega^2\}}{9\omega^4 + (\omega - 2\omega^3)} \leq -1 \quad \text{so the limit is when} \quad -K3\omega^2 = 9\omega^4 + (\omega - 2\omega^3)
\]
Putting \( \omega = 0.707 \) the limiting value of \( K \) is 1.5

**ALTERNATIVE METHOD**

There is another way to solve this and similar problems. The transfer function is broken down into separate components so in the above case we have:
\[
G(s) = \frac{K}{s} \times \frac{1}{1+s} \times \frac{1}{1+2s}
\]
Each is turned into polar co-ordinates (see previous tutorial).
\[
\frac{K}{s} \quad \text{produces a radius of} \quad \frac{K}{\omega} \quad \text{and an angle of} \quad -90^\circ \quad \text{for all radii}
\]
\[
\frac{1}{1+s} \quad \text{produces a radius of} \quad \frac{1}{\sqrt{1+\omega^2}} \quad \text{and angle} \ \tan^{-1}(\omega)
\]
\[
\frac{1}{1+2s} \quad \text{produces a radius of} \quad \frac{1}{\sqrt{1+4\omega^2}} \quad \text{and angle} \ \tan^{-1}2\omega
\]

When we multiply polar coordinates remember that the resultant radius is the product of the individual radii and the resultant angle is the sum of the individual angles. The polar coordinates of the transfer function are then:
\[
\text{Radius} \quad \frac{K}{\omega} \times \frac{1}{\sqrt{1+\omega^2}} \times \frac{1}{\sqrt{1+4\omega^2}} \quad \text{Angle} \quad -90^\circ - \tan^{-1}(\omega) - \tan^{-1}2\omega
\]

Put \( \omega = 0.707 \)
\[
\text{Radius} = 1.414 \times 0.8165 \times 0.577 = 0.667 \quad K \quad \text{Angle} = -90 - 35.26 - 54.74 = -180^\circ
\]

If \( K = 1.5 \) the radius is 1 as stated previously.

© D.J.Dunn
3 PHASE MARGIN and GAIN MARGIN

3.1 PHASE MARGIN

This is the additional phase lag which is needed to bring the system to the limit of stability. In other words it is the angle between the point -1 and the vector of magnitude 1.

3.2 GAIN MARGIN

This is the additional gain required to bring the system to the limit of stability.

WORKED EXAMPLE No.1

The open loop transfer function of a system is $G(s) = \frac{200}{(1+2s)(3+S)(5+S)}$. Produce a polar plot for $\omega = 3$ to $\omega = 10$. Determine the phase and gain margin.

SOLUTION

Evaluate the polar coordinates for $\frac{200}{1 + 2s}$, then $\frac{1}{2+s}$ then $\frac{1}{5+s}$ (See previous tutorial)
Now add the three sets of angles and multiply the three sets of radii and plot the results.

<table>
<thead>
<tr>
<th>( \omega )</th>
<th>( R )</th>
<th>( \phi )</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>5.547</td>
<td>-93.18</td>
</tr>
<tr>
<td>2</td>
<td>2.498</td>
<td>-131.455</td>
</tr>
<tr>
<td>3</td>
<td>1.329</td>
<td>-156.501</td>
</tr>
<tr>
<td>4</td>
<td>0.773</td>
<td>-174.665</td>
</tr>
<tr>
<td>5</td>
<td>0.483</td>
<td>-188.326</td>
</tr>
<tr>
<td>6</td>
<td>0.317</td>
<td>-198.866</td>
</tr>
<tr>
<td>7</td>
<td>0.218</td>
<td>-207.178</td>
</tr>
<tr>
<td>8</td>
<td>0.155</td>
<td>-213.862</td>
</tr>
<tr>
<td>9</td>
<td>0.114</td>
<td>-219.331</td>
</tr>
<tr>
<td>10</td>
<td>0.086</td>
<td>-223.873</td>
</tr>
</tbody>
</table>

The region of interest is where the plot is \(-180^\circ\) and the radius is 1. This would require a much more accurate plot around the region for \( \omega = 3 \) to 5 as shown below.

The phase margin is \(180 - 166 = 14^\circ\)  The gain margin is \(1 - 0.65 = 0.35\)

**SELF ASSESSMENT EXERCISE No.1**

1. Determine the steady state gain and primary time constant for \( G(s) = 10/(s + 5) \). Determine the polar coordinates when \( \omega = 1/T \)
   (Gain = 2 and Radius = 1.414 and angle = \(-45^\circ\))

2. Determine the steady state gain for \( G(s) = 0.5/\{(s+2)(s+10)\} \). Determine the polar coordinates when \( \omega = 0.5 \)
   (Gain = 0.025, \( R_1 = 0.0243 \), \( \phi_1 = -16.9^\circ \))

3. The open loop transfer function of a system is \( G(s) = 80/\{(s+1)(s+2)(s+4)\} \). Produce a polar plot for \( \omega = 3 \) to \( \omega = 10 \). Determine the phase and gain margin (0.11 and 3.5°).
These are logarithmic plots of the magnitude (radius of the polar plot) and phase angle of the transfer function. First consider how to express the gain in decibels.

Strictly \( G \) is a power gain and \( G = \frac{\text{Power out}}{\text{Power In}} \)

If the power in and out were electric then we may say \( G = \frac{V_{\text{out}}}{V_{\text{in}}} \) or \( \frac{I_{\text{out}}}{I_{\text{in}}} \)

Using Ohm’s Law this with the same value of Resistance at input and output this becomes

\[
G = \frac{V_0^2}{V_i^2} \text{ or } \frac{I_0^2}{I_i^2}
\]

Expressing \( G \) in decibels \( G(\text{db}) = 10 \log \frac{V_0^2}{V_i^2} = 20 \log \frac{V_o}{V_i} \text{ or } 20 \log \frac{I_o}{I_i} \)

From this, it is usual to express the modulus of \( G \) as

\[
|G| = 20 \log \left| \frac{0_o}{0_i} \right|
\]

Note that the gain in db is the \( 20 \log R \) where \( R \) is the radius of the polar plot in previous examples.

Consider the transfer function \( G(s) = \frac{1}{s} \)

\[
G(j\omega) = \frac{1}{j\omega} = \frac{-j}{\omega} \quad |G| = \left| \frac{-j}{\omega} \right| = \left| \frac{1}{\omega} \right| \quad G(\text{db}) = 20 \log \left( \frac{1}{\omega} \right) = -20 \log \omega
\]

Plotting this equation produces the following graph. The graph shows a straight line passing through 0 db at \( \omega=1 \) with a gradient of -20 db per decade. The phase angle is -90° at all values of \( \omega \).

Now consider the following transfer function

\[
G(s) = \frac{1}{Ts + 1} \quad |G| = \left| \frac{1}{j\omega T + 1} \right| = \frac{1}{|j\omega T + 1|}
\]

\[
G(j\omega) = \frac{1}{1 + \omega^2 T^2} - j \frac{\omega T}{1 + \omega^2 T^2} \quad \text{The radius of the polar coordinate is } \frac{1}{\sqrt{T^2 \omega^2 + 1}} \text{ and this is the gain.}
\]

The gain in db is then

\[
G(\text{db}) = 20 \left[ \log \left( \frac{1}{\sqrt{T^2 \omega^2 + 1}} \right) \right] = -20 \left[ \frac{1}{2} \log(T^2 \omega^2 + 1) \right] = -10 \log(T^2 \omega^2 + 1)
\]

The phase angle is \( -\tan^{-1}(\omega T) \)
If we put \( T = 1 \) as a convenient example, and plot the result, we get two distinct straight lines shown on the left graph. The horizontal line is produced by very small values of \( \omega \) and so it is called the **LOW FREQUENCY ASYMPTOTE**. The sloping straight line occurs at high values of \( \omega \) and is called the **HIGH FREQUENCY ASYMPTOTE** and has a gradient of -20 db per decade. The two lines meet at the breakpoint frequency or natural frequency given by \( \omega_n = 1/T = 1 \) in this case.

The graph on the right shows phase angle plotted against \( \omega \) and it goes from 0 to \(-90^\circ\). The \( 45^\circ \) point occurs at the break point frequency.

![Graphs showing asymptotes and phase angle](image)

Figure 10

Now consider the following transfer function. (Standard first order response to a step input)

\[
G(s) = \frac{K}{s(1 + sT)} \quad G(j\omega) = \frac{K}{j\omega (1 + j\omega T)}
\]

Note there is an easier way to find \(|G|\) as follows. Separate the two parts and find the modulus of each separately.

\[
|G| = K \frac{1}{|j\omega|} \left| \frac{1}{1 + \omega^2 T^2} \right| = K \left( \frac{1}{\omega} \right) \left( \frac{1}{\sqrt{1 + \omega^2 T^2}} \right)
\]

Taking logs we get

\[
\log |G| = \log K + \log \left( \frac{1}{\omega} \right) + \log \left( \frac{1}{\sqrt{1 + \omega^2 T^2}} \right) = \log K - \log \omega - \frac{1}{2} \log(1 + \omega^2 T^2)
\]

\[
\log |G|db = 20 \left[ \log K - \log \omega - \frac{1}{2} \log(1 + \omega^2 T^2) \right]
\]

There are three components to this and we may plot all three separately as shown. The graph for the complete equation is the sum of the three components. The result is that the graph has two distinctive slopes of -20 db per decade and -40 db per decade. (K and T were taken arbitrarily as 10 giving a breakpoint of \( \omega = 1/T = 0.1 \).

© D.J.Dunn
The plot of phase angle against frequency on the logarithmic scale shows that the phase angle shifts by $90^\circ$ every time it passes through a breakpoint frequency. The plot for the case under examination is shown.

A reasonable result is obtained by sketching the asymptotes for each and adding them together.
WORKED EXAMPLE No. 2

A system has a transfer function \( G(s) = \frac{1}{s(Ts + 1)} \) Where the time constant \( T \) is 0.5 seconds.

Plot the Bode diagram for gain and phase angle. Find the low frequency gain per decade, the high frequency gain per decade and the break point frequency.

SOLUTION

\[
G(s) = \frac{1}{s(Ts + 1)} \quad G(j\omega) = \frac{1}{j\omega} \left( \frac{1}{j\omega T + 1} \right) \quad |G| = \left| \frac{1}{j\omega} \right| \left| \frac{1}{j\omega T + 1} \right| = \left( \frac{1}{\omega} \right) \left( \frac{1}{\omega^2 T^2 + 1} \right)
\]

\[
|G|(db) = 20 \left[ -\log \omega - \frac{1}{2} \log(\omega^2 T^2 + 1) \right] \quad \phi = -90 - \tan^{-1} \left( \frac{1}{\omega T} \right)
\]

<table>
<thead>
<tr>
<th>( \omega )</th>
<th>0.001</th>
<th>0.01</th>
<th>0.1</th>
<th>1.0</th>
<th>10</th>
<th>100</th>
<th>1000</th>
</tr>
</thead>
<tbody>
<tr>
<td>-\log \omega</td>
<td>3</td>
<td>2</td>
<td>1</td>
<td>0</td>
<td>-1</td>
<td>-2</td>
<td>-3</td>
</tr>
<tr>
<td>-\frac{1}{2}\log(\omega^2 T^2+1)</td>
<td>tiny</td>
<td>tiny</td>
<td>tiny</td>
<td>-0.048</td>
<td>-0.707</td>
<td>-1.707</td>
<td>-2.707</td>
</tr>
<tr>
<td>Total Gain (units)</td>
<td>3</td>
<td>2</td>
<td>1</td>
<td>0</td>
<td>-0.048</td>
<td>-1.707</td>
<td>-3.707</td>
</tr>
<tr>
<td>Total Gain db</td>
<td>60</td>
<td>40</td>
<td>20</td>
<td>-0.96</td>
<td>-34.14</td>
<td>-74.14</td>
<td>-114.14</td>
</tr>
<tr>
<td>( \phi ) degrees</td>
<td>-90</td>
<td>-90.3</td>
<td>-92.9</td>
<td>-117</td>
<td>-169</td>
<td>-179</td>
<td>-180</td>
</tr>
</tbody>
</table>

Examining the table we see that the gain drops by 20 db per decade at low frequencies and by 40 db per decade for high frequencies. Plotting the graph on logarithmic paper reveals a breakpoint frequency of 2 rad/s which is also found by \( \omega_n = 1/T = 1/0.5 = 2 \)

A quick way of drawing an approximate Bode plot is to evaluate the gain in db at the breakpoint frequency and draw asymptotes with a slope of -20 db per decade prior to it and -40 db per decade after it. The phase angle may be found by adding the two components.

\[
G(s) = \frac{1}{s(Ts + 1)} \quad G(j\omega) = \frac{1}{j\omega} + \frac{1}{j\omega T + 1}
\]

The phase angle for the first part is the angle of a vector at position \(-1/\omega\) on the j axis which corresponds to \(-90^\circ\).

The phase angle of the second part is the angle of a vector at \(-1\) on the real axis and \(-\omega T\) on the j axis. The two phase angles may be added to produce the overall result.

A quick way to draw the Bode phase plot is to note that the break point frequency occurs at the mid point of the phase shift (-135° in this case) so draw the asymptotes such that they change by -90° at each breakpoint frequency.

Figure 12
GAIN AND PHASE MARGINS FROM THE BODE PLOT

Gain and phase margins may be found from Bode plots as follows. Locate the point where the gain is zero db (unity gain) and project down onto the phase diagram. The phase margin is the margin between the phase plot and -180°.

Locate the point where the phase angle reaches ±180°. Project this back to the gain plot and the gain margin is the margin between this point and the zero db level. If the gain is increased until this is zero, the system becomes unstable.
WORKED EXAMPLE No.3

Draw the asymptotes of the Bode plots for the systems having a transfer function:

\[ G(s) = \frac{K}{(T_1s + 1)(T_2s + 1)} \]

K is 10, T_1 is 2 seconds and T_2 is 0.2 seconds.

Find the value of K which makes the system stable.

**SOLUTION**

The two break point frequencies are 1/T_1 = 1/2 = 0.5 rad/s and 1/T_2 = 1/0.2 = 5 rad/s.

**GAIN**

Locate the two frequencies and draw the asymptotes. The first one is 20 db/decade up to 0.5 rad/s. The second one is -20 db per decade until it intercepts 5 rad/s. From then on it is -40 db per decade.

**PHASE**

The phase angle diagram is no so easy to construct from asymptotes. Locate the break point frequencies. These mark the mid points between 0 and 90° (45°) for both functions. (K has zero angle). The resultant phase angle varies from 0 to -180° reaching -135° half way between the break points.

The phase angle reaches 180° at around \( \omega = 110 \text{ rad/s} \). The gain at 110 rad/s is about -60 db hence the gain margin is about 60 db. To make the gain unity (zero db) we need an extra gain of:

\[ 60 = 20 \log G \quad G = 1000 \]

If the plot is repeated with K = 2 000 it will be seen that the gain margin is about zero.
SELF ASSESSMENT EXERCISE No.2

1. A system has a transfer function

\[ G(s) = \frac{4}{s(Ts + 1)} \]

T is 0.1 seconds.

What is the steady state gain? (4)

What is the low frequency gain per decade, the high frequency gain per decade and the break point frequency? (-20 db, -40 db and 10 rad/s)

2. A system has a transfer function

\[ G(s) = \frac{1}{(T_1s + 1)(T_2s + 1)} \]

T_1 is 0.25 seconds and T_2 is 0.15 seconds.

Find the low frequency gain per decade, the high frequency gain per decade and the break point frequencies. (0 db, -40 db and 4 rad/s and 6.7 rad/s)

Find the gain margin and phase margin. (-80 db and 0° approximately)

3. Draw the asymptotes of the Bode plots for the systems having a transfer function

\[ G(s) = \frac{K}{(T_1s + 1)(T_2s + 1)} \]

K is 2, T_1 is 0.1 seconds and T_2 is 10 seconds.

Find the gain margin and the value of K which makes the system stable. (130 db and 3 x 10^6 approx)

4. The diagram shows the bode gain and phase plot for a system. Determine the gain margin and whether or not the system is stable. (45 db and 10° approx Unstable)